

Thermal bridge calculation for the certification of the window frame PROGRESSION as a suitable component for Passive Houses

for SLAVONA, s.r.o. Stálkovská 258 Slavonice Czech Republic



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1. Introduction

Because a separate heating system is not necessarily required in Passive Houses, high demands are placed on the quality of the building components used. If no radiator under the windows is planned, the thermal transmittance U_W (U-value) of the window used may not exceed 0.80 W/(m²K), in order to prevent unpleasant radiant heat deprivation and cold air descent at the window. For a given quality of glazing, this results in restriction of the thermal bridge loss coefficient for window frames. The following requirements for the certificate "Passive House suitable component" have been set by the PHI:

$U_W \leq 0.80 \text{ W/(m^2K)}$

 U_W is the average thermal transmittance for the whole window. The criterion must be met with $U_g = 0.70 \text{ W}/(m^2\text{K})$ and with a window size of 1.23 m x 1.48 m.

U_{W,installed} ≤ 0.85 W/(m²K)

 $U_{W,installed}$ is the U-Value of the installed window. The criterion must be met in minimum three installation situations.

Also the hygiene criterion must be met. For reasons of hygiene, this criterion limits the minimum individual temperature on window surfaces to prevent mould growth. Criterion for cool, temperate climate is:

$f_{Rsi_0.25\ m^2K/W} \geq 0.70$

At -5 °C ambient temperature, 20 °C interior temperature and 50% relative humidity is the minimum temperature of the surface therefor is limited to 12.6 °C.

In addition, certified windows will be ranked by the thermal losses through the not transparent parts, aligned to Ψ_{opaque} . These efficiency classes include the U-Value of the frame, the frame width, the Ψ -Value of the Glass edge and the length of the Glass edge:

$$\Psi_{opaque} = \Psi_g + \frac{U_f \cdot A_f}{l_g}$$

Relevant for passive houses is the energy balance, the sum out of losses and gains. Because the solar gains are difficult to quote it is useful to rate the parts of the window, which do not allow solar gains. This does Ψ_{opaque} .

Ψ _{opaque}	Passive house efficiency class	Name
≤ 0.110 W/(mK)	_{ph} A	Advanced component
≤ 0.155 W/(mK)	_{ph} B	Basic component
≤ 0.220 W/(mK)	ph C	Certifiable component

Table 1: Passive house efficency classes



2. Guidelines for thermal bridge calculation for windows

On behalf of the SLAVONA, s.r.o. company in Slavonice, the Passive House Institute has calculated the thermal characteristics for a window based on the regulation EN ISO 10077 (standard size 1.23 m * 1.48 m), with an insulated window frame PROGRESSION.

The calculations were carried out using the heat flow software Bisco by the Belgian company Physibel.

2.1 Description of the window frame

Timber frame (Spruce and Thermowood) with insulation ($\lambda = 0.058$ W/mK). Used spacer: SwisspacerV.

2.2 Glass, Panel and Spacer

For triple glazing with low-e coating, generally a Glasss U-value of $U_g = 0.7 \text{ W/(m^2K)}$ is assumed for the calculations in the course of certification. In order to meet the certification criterion $U_W = 0.80 \text{ W/(m^2K)}$, a frame (including spacer and edge bond) with the corresponding thermal quality is necessary

Properties of the	Edge-bond Swisspa	
glazing	Number of panes	3
	Thickness of the panes	4/4/4 mm
	Thickness of the gas gap	18 mm
	Glazing	48 mm
	Conductivity of gas gap	0,029 W/(mK)
	Additional air gap	- mm
	Thickness of additional pane	- mm
	conductivity of air gap	- W/(mK)
	thickness of the total glazing	48 mm
	U-Value of the glazing	0,700 W/(m ² K)
Properties of the	Conductivity of the panel	0,035 W/(mK)
panel	U-Value of the panel	0,649 W/(m ² K)

Table 2: Properties of the glazing and the panel.



In many edge bond constructions, very thin (about 0.025 to 0.1 mm) films are incorporated, the materials of which have a high thermal conductivity. The true-scale representation of the spacer in the calculation model could only be resolved with a very large numerical effort.

Instead of a high resolution representation of the spacer SwisspacerV a simplified, but thermally equivalent, replacement was therefore used. This allows a more coarse discretisation of the calculation model and therefore a viable computational effort.

2.3 Boundary conditions

The boundary conditions for the calculations were chosen to reflect the actual circumstances, i.e. with an external temperaure of -10 °C, an interior temperature of +20 °C and the corresponding heat transfer coefficient at the surfaces (see table below). A reduced inner heat transfer coefficient of $h_i = 5 \text{ W/(m^2K)}$ was assumed at the inner surfaces of the window corners, in accordance with DIN EN 10077-2.

Surface	Temperature θ [℃]	Heat-transfer resistance R _{si} [m²K/W]
to ambient	10	0.04
to ambient with air gap	-10	0.13
to interior	20	0.13
to interior in edges	20	0.20
to ambient for calculation of f _{Rsi}		0.04
to interior for calculation of f _{Rsi}		0.25

Table 3: Heat transfer resistances and surface temperatures.

2.4 Used materials and thermal conductivities

In the following table the materials used in the calculation are listed with their thermal conductivities and the colours used to represent them. The thermal conductivities are based on information provided by the company or on established standards. The equivalent thermal conductivity of hollow spaces was determined in accordance with DIN EN 10077-2.



Table 4: Thermal conductivities and colours representing the materials used for the calculation model.

Farbe	λ	Description
Coulour	W/mK	
	0,035	Insulation material
	0,040	Insulation material
	0,041	PE-Strip
	0,050	PU in-situ foam
	0,050	Soft wood fibre board
	0,058	Cork
	0,100	Molecular sieve
	0,110	Spruce
	0,116	Thermowood Pine
	0,130	Softwood ~500kg/m³, OSB ~650kg/m³
	0,180	Hardwood ~700kg/m ³
	0,190	Swisspacer V replacement
	0,190	Glass fibre reinforced plastic
	0,230	Fiberglas
	0,250	Plasterboard
	0,250	EPDM
	0,289	Polybutyl
	0,290	2,2x Softwood ~500kg/m ³ (heat flow in direction of fibres)
	0,350	Silicone
	0,400	Polysulphide
	0,510	Interior plaster/gypsum board
	0,700	Exterior plaster
	1,0	Sand-lime brick
	1,0	Glass
	2,3	Reinforced concrete
	3,5	Marble
	50	Steel
	160	Aluminium silicum alloy



3. Results of the heat-flow-calculation

The heat flow Q_{total} was calculated for each sectional drawing following DIN EN 10077–1 and 2 using the two-dimensional heat flow software programme Bisco. For each section, two calculations were carried out, one with the installed glazing and one with a calibration panel (lamda-value of 0,035 W/(m²K)) in place of the glazing. The depth of the edge and thickness of the calibration panel correspond with those of the glazing. Each of the calculated heat flow Q_{total} are documented with the respective dimensions of the sections in Table 3. These intermediate results form the basis for the calculation of the U-values and the Ψ -values.

The height of the calculation models is 0.4 m in models with one glazed part and 0.6 m in models with two glazed parts. For installation situations 1.41 m.

Name		Progression			
nel	bottom	8,3020			
ı pa	top	8,2779			
with	side	8,2779			
tme	mullion	12,5111			
Fra	-				
Edge boi	nd	SwisspacerV			
ass	bottom	9,5165			
with gla	top	9,5198			
	side	9,5198			
ame	mullion	14,7195	 		
Fra	-				
(A)	bottom	13,8335			
EIE EIE	top	13,4051			
	side	13,4051	 		
	bottom	14,0765	 		
Timbe const wall	top	13,9064	 		
	side	13,9064			
a ted	bottom	13,7731	 		
ntila acin	top	13,5421			
Vei fi	side	13,5421			

Table 5: Results of the heat flow calculations for all sections [W/m].



4. Overview of calculation results

Table 6: Overview of calculation results.

Name		Progression				
b₁	bottom	0,109				
dth	top	0,089				
j≊ [⊓]	side	0,089				
ame	mullion	0,164				
fra	-					
he	bottom	0,807				
² K) ⊂f	top	0,833				
lue ame /(m	side	0,833				
-val fra	mullion	0,818				
\supset	-					
Edge boi	nd	SwisspacerV				
7 ⁴	bottom	0,0256				
ур Г	top	0,0255				
hoi /(m	side	0,0255				
d . [[∑]	mullion	0,0256				
ec ₽	-					
-9- ,25	bottom	0,72				
um Ituri ^{8si=0}	top	0,72				
nim vera r f _F	side	0,72				
amp Icto	mullion	0,72				
fa	-					
Window-	U-value U _w	0,798				
[W/(m ² K]	1/(m/)	, 0.100				
Ψ _{opaque} [V		0,109				
Passive I	House	mh A				
LINCIENC	y class	pii A				
Therma	installation	bridge Ψ _{install}	[W/(mK)] und	U _{W,installed} [W	/(m²K)]	
(0	ton	0,0098				
E .	side	-0,0048				
ш		-0,0048				
	W,installed	0,793				
er wa	ton	0,0139				
mbe str. v	side	0,0139				
i Li		0,0139				
	-w,installed	0.0076				
atec	top	-0.0003				
ntilé acir	side	-0.0003				
e fi		0.802				
	- w,installed	0,001				



5. Certified window construction

In the following figures, the calculation models are shown on the left. The respective isothermal figures are shown on the right. The heat flows perpendicular to the isotherms in colour, as indicated by the black lines. The heat flow rate between the lines is 0.1 W/m. In order to better represent the details, only relevant sections of the calculation model are shown.

Figure 1 shows the sections 'top/side' und 'bottom' of the certified window with a 48 mm wide glazing (4/18/4/18/4) and the spacer SwisspacerV.



Figure 1: Progression: Section 'side/top' and bottom' with the respective isothermal- and heat flux graphic.



5.1 Mullion

Figure 2 shows the section of a mullion of the certified window system with a 48 mm wide glazing (4/18/4/18/4) and the spacer SwisspacerV.

The thermal properties of this section are given for information only. They are not part in the calculation of the window U-value.



Figure 2: Section of the mullion of the window system with respective isothermal and heat flux graphic.



6. Window U-values for different window sizes

The U-value U_W of an uninstalled window of any size can be determined using the following equation:

$$U_{W} = \frac{A_{g} \cdot U_{g} + A_{f} \cdot U_{f} + l_{g} \cdot \Psi_{g}}{A_{g} + A_{f}}$$

where: A_g

- Average glazing U-value [W/(m²K]
- U_f Average frame U-value [W/(m²K]
- I_g Length of edge bond [m] Ψ_g
- Av. th. bridge of edge bond [W/(mK)]



7. Installation

Besides the heat transfer through window frames and glazing, the connection of the frame to a suitable Passive House wall construction is of considerable importance for the whole system (the U-value of the wall must be less than 0.15 W/(m^2 K)). Therefore, three typical installation situations (the specific arrangement of which were given by the manufacturer) were tested for their suitability.

The results are shown in table 5 and 6. For the calculation models and the respective isothermal graphics, see the following pages.

The U-value of an installed window of any size can be determined using the following equation:

. - .

$$\begin{split} U_{W,installed} &= \frac{A_W \cdot U_W + l_{instal.} \cdot \Psi_{instal.}}{A_W} \\ \text{where: } A_W & \text{Window area } [\text{m}^2] & \text{U}_W & \text{Window-U-value } [\text{W}/(\text{m}^2\text{K})] \\ I_{\text{instal.}} & \text{Length of installation } [\text{m}] & \Psi_{\text{instal.}} & \text{Av. th. installation bridge } [\text{W}/(\text{mK})] \end{split}$$



7.1 Exterieur Wall with Insulation and Finnishing-System (EIFS)

The following figure shows the installation of the Progression 'side/top' and 'bottom' in a Exterieur Wall with Insulation and Finnishing-System (EIFS).

The respective isothermal figures are shown on the right. The heat flows perpendicular to the isotherms in colour, as indicated by the black lines. The heat flow rate between the lines is 0.1 W/m.

In order to better represent the details, only relevant sections of the calculation model are shown.



Figure 3: Installation 'bottom' und 'side/top' in a Exterieur Wall with Insulation and Finnishing-System (EIFS) with respective isothermal graphic

	U wall	Ψ _{instal., bottom}	Ψ _{instal., s./top}	U _{w,installed}
	[W/(m²K)]	[W/(mK)]	[W/(mK)]	[W/(m²K)]
Progression	0,133	0,010	-0,005	0,79



7.2 Timber construction wall

The following figure shows the installation of the Progression 'top/side' und 'bottom' in a Timber construction wall.

The respective isothermal figures are shown on the right. The heat flows perpendicular to the isotherms in colour, as indicated by the black lines. The heat flow rate between the lines ist 0.1 W/m.

In order to better represent the details, only relevant sections of the calculation model are shown.



Figure 4: Installation 'bottom' und 'side/top' in a Timber construction wall with respective isothermal graphic

	U wall	Ψ _{instal., bottom}	Ψ _{instal., s./top}	U _{W,installed}
	[W/(m²K)]	[W/(mK)]	[W/(mK)]	[W/(m²K)]
Progression	0,131	0,020	0,014	0,84



7.3 Ventilated facing

The following figure shows the installation of the Progression 'side/top' and 'bottom' in a Ventilated facing.

The respective isothermal figures are shown on the right. The heat flows perpendicular to the isotherms in colour, as indicated by the black lines. The heat flow rate between the lines ist 0.1 W/m.

In order to better represent the details, only relevant sections of the calculation model are shown.



Figure 5: Installation 'bottom' and 'side/top' in a Ventilated facing with respective isothermal graphic

	U wall	Ψ _{instal., bottom}	Ψ _{instal., s./top}	U _{w,installed}
	[W/(m²K)]	[W/(mK)]	[W/(mK)]	[W/(m²K)]
Progression	0,133	0,008	0,000	0,80



8. Final evaluation

The present PROGRESSION of the SLAVONA, s.r.o. company is a successfull and effective construction of a Passive House suitable component in therms of the tested parameters.

Due to the use of the spacer SwisspacerV the criteria are reached.

The results of the heat flow calculations, which are documented in this report, prove that the values required for U_W and $U_{W,\text{installed}}$ are met.

During the construction care should be taken that the windows are installed as stated in the report, otherwise the thermal bridge heat loss coefficient for the installation may be considerably worse.



9. Appendix: Construction drawings

Progression: Frame sections 'bottom' (not to scale)





Progression: Frame sections 'side/top' (not to scale)









Progression: Installation in a Exterieur Wall with Insulation and Finnishing-System (EIFS) (not to scale)





Progression: Installation in a Timber construction wall (not to scale)





Progression: Installation in a ventilated facing (not to scale)

